## Electrical Technology (EE-101F)

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- Introduction about three phase
- Three phase voltage \& current
- Power Relations
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## Introduction

Almost all electric power generation and most of the power transmission in the world is in the form of three-phase AC circuits. A three-phase AC system consists of three-phase generators, transmission lines, and loads.

There are two major advantages of three-phase systems over a single-phase system:

1) More power per kilogram of metal form a three-phase machine;
2) Power delivered to a three-phase load is constant at all time, instead of pulsing as it does in a single-phase system.

The first three-phase electrical system was patented in 1882 by John Hopkinson -_British physicist, electrical engineer, Fellow of the Royal Society.

## Three-phase voltages and currents

A three-phase
generator consists of
three single-phase
generators with
voltages of equal
amplitudes and
phase differences of
$120^{\circ}$.


$$
\begin{aligned}
v_{A}(t) & =\sqrt{2} V \sin \omega t \mathrm{~V} \\
\mathbf{V}_{A} & =V \angle 0^{\circ} \mathrm{V} \\
v_{B}(t) & =\sqrt{2} V \sin \left(\omega t-120^{\circ}\right) \mathrm{V} \\
\mathbf{V}_{B} & =V \angle-120^{\circ} \mathrm{V} \\
v_{C}(t) & =\sqrt{2} V \sin \left(\omega t-240^{\circ}\right) \mathrm{V} \\
\mathbf{V}_{C} & =V \angle-240^{\circ} \mathrm{V}
\end{aligned}
$$



## Three-phase voltages and currents

Each of three-phase generators can be connected to one of three identical loads.

This way the system would consist of three single-phase circuits differing in phase angle by $120^{\circ}$.

The current flowing to each load can be found as

$$
I=\frac{V}{Z}
$$



## Three-phase voltages and currents

Therefore, the currents flowing in each phase are


## Three-phase voltages and currents

We can connect the negative (ground) ends of the three singlephase generators and loads together, so they share the common return line (neutral).


## Three-phase voltages and currents

The current flowing through a neutral can be found as

$$
\begin{equation*}
I_{N}=I_{A}+I_{B}+I_{C}=I \angle-\theta+I \angle-\theta-120^{\circ}+I \angle-\theta-240^{\circ} \tag{.1}
\end{equation*}
$$

$=I \cos (-\theta)+j I \sin (-\theta)+I \cos \left(-\theta-120^{\circ}\right)+j I \sin \left(-\theta-120^{\circ}\right)+I \cos \left(-\theta-240^{\circ}\right)+j I \sin \left(-\theta-240^{\circ}\right)$
$=I\left[\cos (-\theta)+\cos \left(-\theta-120^{\circ}\right)+\cos \left(-\theta-240^{\circ}\right)\right]+j I\left[\sin (-\theta)+\sin \left(-\theta-120^{\circ}\right)+\sin \left(-\theta-240^{\circ}\right)\right]$
$=I\left[\cos (-\theta)+\cos (-\theta) \cos \left(120^{\circ}\right)+\sin (-\theta) \sin \left(120^{\circ}\right)+\cos (-\theta) \cos \left(240^{\circ}\right)+\sin (-\theta) \sin \left(240^{\circ}\right)\right]$
$+j I\left[\sin (-\theta)+\sin (-\theta) \cos \left(120^{\circ}\right)-\cos (-\theta) \sin \left(120^{\circ}\right)+\sin (-\theta) \cos \left(240^{\circ}\right)-\cos (-\theta) \sin \left(240^{\circ}\right)\right]$

Which is:

$$
\begin{aligned}
{ }_{N} & =I\left[\cos (-\theta)-\frac{1}{2} \cos (-\theta)+\frac{\sqrt{3}}{2} \sin (-\theta)-\frac{1}{2} \cos (-\theta)-\frac{\sqrt{3}}{2} \sin (-\theta)\right] \\
& +j I\left[\sin (-\theta)-\frac{1}{2} \sin (-\theta)+\frac{\sqrt{3}}{2} \cos (-\theta)-\frac{1}{2} \sin (-\theta)-\frac{\sqrt{3}}{2} \cos (-\theta)\right] \\
& =0
\end{aligned}
$$

## Three-phase voltages and currents

Such three-phase power systems (equal magnitude, phase differences of $120^{\circ}$, identical loads) are called balanced.

In a balanced system, the neutral is unnecessary!
Phase Sequence is the order in which the voltages in the individual phases peak.


## Voltages and currents

There are two types of connections in three-phase circuits: $Y$ and $\Delta$.


Each generator and each load can be either Y - or $\Delta$-connected. Any number of Y - and $\Delta$-connected elements may be mixed in a power system.

Phase quantities - voltages and currents in a given phase.
Line quantities - voltages between the lines and currents in the lines connected to the generators.

## Voltages and currents

## Assuming a resistive load...



## Voltages and currents

$$
\begin{align*}
& V_{a n}=V_{\phi} \angle 0^{0} \\
& V_{b n}=V_{\phi} \angle-120^{\circ}  \tag{.1}\\
& V_{c n}=V_{\phi} \angle-240^{\circ}
\end{align*}
$$

Since we assume a resistive load:

$$
\begin{align*}
& I_{a}=I_{\phi} \angle 0^{\circ} \\
& I_{b}=I_{\phi} \angle-120^{\circ}  \tag{.2}\\
& I_{c}=I_{\phi} \angle-240^{\circ}
\end{align*}
$$

## Voltages and currents

The current in any line is the same as the current in the corresponding phase.

$$
\begin{equation*}
I_{L} \quad I_{\phi} \tag{.1}
\end{equation*}
$$

## Voltages are:

$$
\begin{aligned}
V_{a b} & =V_{a}-V_{b}=V_{\phi} \angle 0^{0}-V_{\phi} \angle-120^{0}=V_{\phi}-\left(-\frac{1}{2} V_{\phi}-j \frac{\sqrt{3}}{2} V_{\phi}\right)=\frac{3}{2} V_{\phi}+j \frac{\sqrt{3}}{2} V_{\phi} \\
& =\sqrt{3} V_{\phi}\left(\frac{\sqrt{3}}{2}+j \frac{1}{2}\right)=\sqrt{3} V_{\phi} \angle 30^{0}
\end{aligned}
$$

## Voltages and currents

Magnitudes of the line-to-line voltages and the line-to-neutral voltages are related as:

$$
V_{u}=\sqrt{3} V_{d}
$$

In addition, the line voltages are shifted by $30^{\circ}$ with respect to the phase voltages.

In a connection with abc sequence, the voltage of a line leads the phase voltage.


## Voltages and currents



$$
\begin{aligned}
& V_{a b}=V_{\phi} \angle 0^{0} \\
& V_{b c}=V_{\phi} \angle-120^{\circ} \\
& V_{c a}=V_{\phi} \angle-240^{\circ}
\end{aligned}
$$

$$
\begin{aligned}
& I_{a b}=I_{\phi} \angle 0^{0} \\
& I_{b c}=I_{\phi} \angle-120^{\circ} \\
& I_{c a}=I_{\phi} \angle-240^{\circ}
\end{aligned}
$$

## Voltages and currents

$$
\begin{equation*}
V_{L L}=V_{\phi} \tag{.1}
\end{equation*}
$$

The currents are:

$$
\begin{align*}
I_{a} & =I_{a b}-I_{c a}=I_{\phi} \angle 0^{0}-I_{\phi} \angle 240^{\circ}=I_{\phi}-\left(-\frac{1}{2} I_{\phi}+j \frac{\sqrt{3}}{2} I_{\phi}\right) \\
& =\frac{3}{2} I_{\phi}-j \frac{\sqrt{3}}{2} I_{\phi}=\sqrt{3} I_{\phi}\left(\frac{\sqrt{3}}{2}-j \frac{1}{2}\right)=\sqrt{3} I_{\phi} \angle-30^{\circ} \tag{.2}
\end{align*}
$$

## Voltages and currents

For the connections with the abc phase sequences, the current of a line lags the corresponding phase current by $30^{\circ}$ (see Figure below).


For the connections with the acb phase sequences, the line current leads the corresponding phase current by $30^{\circ}$.

## Power relationships

For a balanced $Y$-connected load with the impedance $Z_{\phi}=Z \angle \theta$ :

## and voltages:

$$
\begin{align*}
v_{a n}(t) & =\sqrt{2} V \sin \omega t \\
v_{b n}(t) & =\sqrt{2} V \sin \left(\omega t-120^{\circ}\right) \\
v_{c n}(t) & =\sqrt{2} V \sin \left(\omega t-240^{\circ}\right) \tag{3.17.1}
\end{align*}
$$

The currents can be found:

$$
\begin{aligned}
& i_{a}(t)=\sqrt{2} I \sin (\omega t-\theta) \\
& i_{b}(t)=\sqrt{2} I \sin \left(\omega t-120^{\circ}-\theta\right) \\
& i_{c}(t)=\sqrt{2} I \sin \left(\omega t-240^{\circ}-\theta\right)
\end{aligned}
$$



## Power relationships

For a balanced $Y$-connected load with the impedance $Z_{\phi}=Z \angle \theta$ :

## and voltages:

$$
\begin{align*}
& v_{a n}(t)=\sqrt{2} V \sin \omega t \\
& v_{b n}(t)=\sqrt{2} V \sin \left(\omega t-120^{\circ}\right) \\
& v_{c n}(t)=\sqrt{2} V \sin \left(\omega t-240^{\circ}\right) \tag{1}
\end{align*}
$$

The currents can be found:

$$
\begin{aligned}
& i_{a}(t)=\sqrt{2} I \sin (\omega t-\theta) \\
& i_{b}(t)=\sqrt{2} I \sin \left(\omega t-120^{\circ}-\theta\right) \\
& i_{c}(t)=\sqrt{2} I \sin \left(\omega t-240^{\circ}-\theta\right)
\end{aligned}
$$



## Power relationships

## The instantaneous power is:

$$
\begin{equation*}
p(t)=v(t) i(t) \tag{.1}
\end{equation*}
$$

Therefore, the instantaneous power supplied to each phase is:

$$
\begin{align*}
& p_{a}(t)=v_{a n}(t) i_{a}(t)=2 V I \sin (\omega t) \sin (\omega t-\theta) \\
& p_{b}(t)=v_{b n}(t) i_{b}(t)=2 V I \sin \left(\omega t-120^{\circ}\right) \sin \left(\omega t-120^{\circ}-\theta\right)  \tag{.2}\\
& p_{c}(t)=v_{c n}(t) i_{c}(t)=2 V I \sin \left(\omega t-240^{\circ}\right) \sin \left(\omega t-240^{\circ}-\theta\right)
\end{align*}
$$

Since

$$
\begin{equation*}
\sin \alpha \sin \beta=\frac{1}{2}[\cos (\alpha-\beta)-\cos (\alpha+\beta)] \tag{3}
\end{equation*}
$$

## Power relationships

## Therefore

$$
\begin{align*}
& p_{a}(t)=V I[\cos \theta-\cos (2 \omega t-\theta)] \\
& p_{b}(t)=V I\left[\cos \theta-\cos \left(2 \omega t-240^{\circ}-\theta\right)\right]  \tag{1}\\
& p_{c}(t)=V I\left[\cos \theta-\cos \left(2 \omega t-480^{\circ}-\theta\right)\right]
\end{align*}
$$

The total power on the load

$$
\begin{equation*}
p_{\text {tot }}(t)=p_{a}(t)+p_{b}(t)+p_{c}(t)=3 V I \cos \theta \tag{2}
\end{equation*}
$$

The pulsing components cancel each other because of $120^{\circ}$ phase shifts.

## Power relationships

The instantaneous
power in phases.
The total power
supplied to the load is
constant.


## Power relationships

Real

$$
\begin{equation*}
P=3 V_{\phi} I_{\phi} \cos \theta=3 I_{\phi}^{2} Z \cos \theta \tag{1}
\end{equation*}
$$

## Reactive

$$
\begin{equation*}
Q=3 V_{\phi} I_{\phi} \sin \theta=3 I_{\phi}^{2} Z \sin \theta \tag{2}
\end{equation*}
$$

Apparent

$$
\begin{equation*}
S=3 V_{\phi} I_{\phi}=3 I_{\phi}^{2} Z \tag{3}
\end{equation*}
$$

Note: these equations are valid for balanced loads only.

## Power relationships

## Power consumed by a load:

Since for this load

$$
\begin{equation*}
P=3 V_{\phi} I_{\phi} \cos \theta \tag{1}
\end{equation*}
$$

$$
\begin{equation*}
I_{L}=I_{\phi} \text { and } V_{L L}=\sqrt{3} V_{\phi} \tag{2}
\end{equation*}
$$

Therefore:

$$
\begin{align*}
& P=3 \frac{V_{L L}}{\sqrt{3}} I_{L} \cos \theta  \tag{3}\\
& P=\sqrt{3} V_{L L} I_{L} \cos \theta \tag{4}
\end{align*}
$$

Note: these equations are valid for balanced loads only.

## Power relationships

## Power consumed by a load:

$$
\begin{equation*}
P=3 V_{\phi} I_{\phi} \cos \theta \tag{1}
\end{equation*}
$$

Therefore:

$$
\begin{equation*}
P=3 \frac{I_{L}}{\sqrt{3}} V_{L L} \cos \theta \tag{.3}
\end{equation*}
$$

$$
\begin{equation*}
I_{L}=\sqrt{3} I_{\phi} \text { and } V_{L L}=V_{\phi} \tag{.2}
\end{equation*}
$$

$$
\begin{equation*}
P=\sqrt{3} V_{L L} I_{L} \cos \theta \tag{4}
\end{equation*}
$$

Note: these equations were derived for a balanced load.

## Power relationships

Reactive power

$$
\begin{equation*}
Q=\sqrt{3} V_{L L} I_{L} \sin \theta \tag{1}
\end{equation*}
$$

Apparent power

$$
\begin{equation*}
S=\sqrt{3} V_{L L} I_{L} \tag{2}
\end{equation*}
$$

Note: $\theta$ is the angle between the phase voltage and the phase current - the impedance angle.

## Anatysis of balanced systems

We can determine voltages, currents, and powers at various points in a balanced circuit.

Consider a Y-connected generator and load via three-phase transmission line.

For a balanced Y-connected system, insertion of a neutral does not change the system.
All three phases are identical except of $120^{\circ}$ shift. Therefore, we can analyze a single phase (per-phase circuit).

Limitation: not valid for $\Delta$-connections...


## Anatysis of balanced systems

A $\Delta$-connected circuit can be analyzed via the transform of impedances by the Y- $\Delta$ transform. For a balanced load, it states that a $\Delta$-connected load consisting of three equal impedances $Z$ is equivalent to a $Y$-connected load with the impedances $Z / 3$. This equivalence implies that the voltages, currents, and powers supplied to both loads would be the same.


## Anatysis of balanced systems: Ex

Example 3-1:
for a 208-V threephase ideally balanced system, find:
a) the magnitude of the line current $I_{L}$;
b) The magnitude of the load's line and phase voltages $V_{L L}$ and $V_{\phi L}$;
c) The real, reactive, and the apparent powers consumed by the load;
d) The power factor of the load.


$$
\mathbf{v}_{\varphi}=\frac{V_{L}}{\sqrt{3}}=\frac{208}{\sqrt{3}}=120 \mathrm{~V}
$$

## Analysis of balanced systems: Ex

Both, the generator and the load are $Y$ connected, therefore, it's easy to construct a per-phase equivalent circuit...

a) The line current:
$I_{L}=\frac{V}{Z_{L}+Z_{\text {load }}}=\frac{120 \angle 0^{0}}{(0.06+j 0.12)+(12+j 9)}=\frac{120 \angle 0^{0}}{12.06+j 9.12}=\frac{120 \angle 0^{0}}{15.12 \angle 37.1^{0}}=7.94 \angle-37.1^{0} \quad \mathrm{~A}$
b) The phase voltage on the load:

$$
V_{\phi L}=I_{\phi L} Z_{\phi L}=\left(7.94 \angle-37.1^{0}\right)(12+j 9)=\left(7.94 \angle-37.1^{0}\right)\left(15 \angle 36.9^{0}\right)=119.1 \angle-0.2^{0} V
$$

The magnitude of the line voltage on the load:

$$
V_{L L}=\sqrt{3} V_{\phi L}=206.3 \mathrm{~V}
$$

## Anatysis of balanced systems: Ex



The apparent power consumed by the load:

$$
S_{\text {load }}=3 V_{\phi} I_{\phi}=3 \cdot 119.1 \cdot 7.94=2839 \mathrm{VA}
$$

d) The load power factor:

$$
P F_{\text {load }}=\cos \theta=\cos 36.9^{0}=0.8-\text { lagging }
$$

## Using the power triangle

If we can neglect the impedance of the transmission line, an important simplification in the power calculation is possible...

If the generator voltage in the system is known, then we can find the current and power factor at any point in the system as follows:

1. The line voltages at the generator and the loads will be identical since the line is lossless.
2. Real and reactive powers on each load.
3. The total real and reactive powers supplied to all loads from the point examined.
4. The system power factor at that point using the power triangle relationship.
5. Line and phase currents at that point.



(a) A Y-connected $3-1$ source

(b) The phase and line yotage phasor dlagram tor a Y Y connected $\$=\phi$ source

A Y-connected $3-\phi$ source and its voltage phasor diagram

$$
\begin{aligned}
& \mathbf{v}_{a b}=\mathbf{v}_{a}-\mathbf{v}_{b}=\sqrt{3} V_{\mathrm{Y}} \angle 30^{\circ} \\
& \mathbf{v}_{b c}=\mathbf{v}_{b}-\mathbf{v}_{c}=\sqrt{3} V_{\mathrm{Y}} \angle-90^{\circ} \\
& \mathbf{v}_{c a}=\mathbf{v}_{c}-\mathbf{v}_{a}=\sqrt{3} V_{\mathrm{Y}} \angle+150^{\circ}
\end{aligned}
$$

the relationship between the phase (or line-to-neutral) voltages and the line (or line-to-line) voltages can be written as follows:

$$
V_{l}=\sqrt{3} V_{\mathrm{Y}} \quad \text { and } \quad \mathbf{I}_{l}=\mathbf{I}_{\mathrm{Y}}
$$


(a) A A-connected $3-\phi$ source

(b) The phase and line current phasor diagram


A $\Delta$-connected 3- $\phi$ source and its current phasor diagram

$$
\begin{aligned}
\mathbf{I}_{a} & =\mathbf{I}_{a b}-\mathbf{I}_{c a}=\sqrt{3} I_{\Delta} \angle-30^{\circ} \\
\mathbf{I}_{b} & =\mathbf{I}_{b c}-\mathbf{I}_{a b}=\sqrt{3} I_{\Delta} \angle-150^{\circ} \\
\mathbf{I}_{c} & =\mathbf{I}_{c a}-\mathbf{I}_{b c}=\sqrt{3} I_{\Delta} \angle+90^{\circ}
\end{aligned}
$$

Note that for a $\Delta$-connected three-phase source, the amplitudes of line currents are $\sqrt{3}$ times that of phase currents and the line voltage is the same as the phase voltage:

$$
I_{I}=\sqrt{3} I_{\Delta}
$$

and

$$
\mathbf{V}_{l}=\mathbf{V}_{\Delta}
$$

## Measurement of Three-Phase Power

three-phase power can be measured using just two wattmeters.

(a) Two-watmeter connection to measure a three-phase AC power

(b) The phasor diagrams for voltages/currents

From the connections shown in fig (a) above, the readings of the two wattmeters can be written as

$$
\begin{aligned}
& P_{1}=V_{a b} I_{a} \cos \left(\theta+30^{\circ}\right) \\
& P_{2}=V_{c b} I_{c} \cos \left(\theta-30^{\circ}\right)
\end{aligned}
$$

From the phasor diagram shown in fig (b) above, the sum of these two readings gives the three phase active power

$$
\begin{aligned}
P_{1}+P_{2} & =V_{a b} I_{a} \cos \left(\theta+30^{\circ}\right)+V_{c b} I_{c} \cos \left(\theta-30^{\circ}\right) \\
& =V_{l} I_{l} \cos \left(\theta+30^{\circ}\right)+V_{l} I_{l} \cos \left(\theta-30^{\circ}\right)
\end{aligned}
$$

